

# MOHID-GLM : code developments for 3D waves-current interactions

Implementation of the glm2-RANS equations by Ardhuin et al. 2008

MOHIDing workshop – 7-8 June, 2018 – Lisbon, Portugal

**Matthias Delpey - SUEZ**

Center Rivages Pro Tech  
matthias.delpey@rivagesprotech.fr



# Motivations

## Need for 3D wave-current implementation

- 3D features in the flow may be generated by multiple factors
  - Density stratification by continental freshwater outflows
  - Wind-induced circulation
  - Vertical shear in rip currents
  
- Surface gravity waves have a large impact on nearshore circulation in energetic environments
  - Wave setup
  - Longshore currents
  - Rip currents
  - Horizontal & vertical mixing
  - Etc.

➔ **Need for 3D models including the effect of waves**

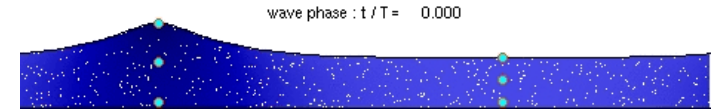


# Issue

## The difficulty of including waves in phase-averaged 3D models

- Decomposition of flow components

$$\mathbf{u} = \underbrace{\langle \mathbf{u} \rangle}_{\text{vitesse moyenne}} + \underbrace{\tilde{\mathbf{u}}}_{\text{vitesse oscillante}} + \underbrace{\mathbf{u}'}_{\text{vitesse turbulente}}$$
$$\mathbf{m}^T = \underbrace{\mathbf{m}}_{\text{qdm du courant sous-jacent}} + \underbrace{\mathbf{m}^W}_{\text{qdm résiduelle des vagues}}$$

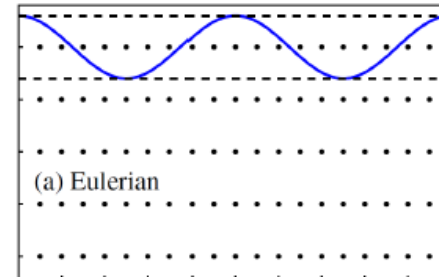


→ Objective = representing interactions between mean flow and oscillating flow (momentum, mass, energy)

- Problem: it is difficult to apply an Eulerian average on phases in 3D

$$\overline{\phi(\mathbf{x}, t)} = \frac{1}{T} \int_{-T/2}^{T/2} \phi(\mathbf{x}, t + t') dt'$$

$$\Rightarrow \frac{1}{T} \int_{-T/2}^{T/2} \phi(\mathbf{x} + \xi, t + t') dt'$$



# The Generalized Lagrangian Mean approach

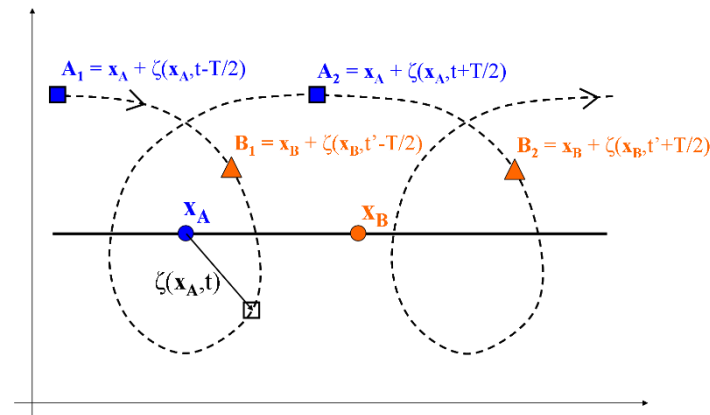
## Main principle

- Derive new equations using a Lagrangian coordinate change, from the mean position  $X$  to the instantaneous position  $X + \xi$
- Allows to « follow » the oscillatory movement
- Generalized Lagrangian Mean (Andrews & McIntyre, 1978)

$$\overline{\phi(x, t)}^L = \overline{\phi(x + \zeta(x, t), t)}$$

- New mean advection velocity + new Lagrangian derivation operator
- Application of the GLM to the RANS equations

- Arduin et al. 2008 : asymptotic formulation of GLM equations for surface gravity waves → Development order 2
  - Small wave steepness
  - Limited vertical shear of the mean current
  - Slowly varying propagation environment



$$\overline{u(x, t)}^L$$

$$\overline{D}^L \phi = \frac{\partial \phi}{\partial t} + \overline{u}_i^L \frac{\partial \phi}{\partial x_i}$$

# The Generalized Lagrangian Mean approach

## GLM2-RANS equations

### ○ Momentum equation

$$\frac{\partial \underline{u}}{\partial t} + \frac{\partial \underline{u}\underline{u}}{\partial x} + \frac{\partial v\underline{u}}{\partial y} + \frac{\partial w\underline{u}}{\partial z} - f\underline{v} \frac{1}{\rho} \frac{\partial p^H}{\partial x} = fV_s + \frac{\partial \underline{u}}{\partial x} U_s + \frac{\partial v}{\partial x} V_s - \frac{\partial J}{\partial x} + F_{m,x} + F_{d,x}$$

where:  $\underline{u}$  is now the GLM velocity (= tracer advection velocity)

$U_s, V_s$  = Stokes drift components

$\underline{u} = u - U_s$  = quasi-Eulerian current

$p^H$  = hydrostatic pressure

$J$  = wave-induced pressure (barotropic)

$F_{m,x}$  = momentum flux from the turbulent mixing

$F_{d,x}$  = momentum flux induced by wave breaking

$f$  = Coriolis parameter

# The Generalized Lagrangian Mean approach

## GLM2-RANS equations

○ Wave induced pressure  $J = g \frac{kE}{\sinh(2kD)}$

○ 3D Stokes drift  $(U_s, V_s) = \sigma k (\cos \theta, \sin \theta) E \frac{\cosh(2kz + 2kh)}{\sinh^2(kD)}$

○ Wave-breaking induced flux of momentum:  $(\tau_{oc,x}, \tau_{oc,y}) = \rho_w \cdot \int \frac{g}{C(f, \theta)} (\cos \theta, \sin \theta) S_{oc}(f, \theta) df d\theta$

→ Given by the wave model as an input to MOHID

# The Generalized Lagrangian Mean approach

## GLM2-RANS equations

### ○ Mass equation

$$\frac{\partial \bar{\eta}}{\partial t} + \frac{\partial D(\bar{u} + \bar{U}_s)}{\partial x} + \frac{\partial D(\bar{v} + \bar{V}_s)}{\partial y} = 0$$

where:  $u$  is now the GLM velocity (= tracer advection velocity)

$U_s, V_s$  = Stokes drift components

$\bar{\eta}$  mean free surface elevation

$D$  total water depth

upper bar = vertical integration

# The Generalized Lagrangian Mean approach

## GLM2-RANS equations

○ Surface boundary condition

$$\frac{\partial \eta}{\partial t} + (\underline{u} + U_s) \frac{\partial \eta}{\partial x} + (\underline{v} + V_s) \frac{\partial \eta}{\partial y} = \underline{w} + W_s$$

$$K_M \frac{\partial \underline{u}_\alpha}{\partial z} = \tau_{a,\alpha} - \tau_{aw,\alpha}$$

○ Bottom boundary condition

$$\underline{u} \frac{\partial h}{\partial x} + \underline{v} \frac{\partial h}{\partial y} = \underline{w}$$

$$K_M \frac{\partial \underline{u}_\alpha}{\partial t} = \rho C_D |\underline{u}| \underline{u}_\alpha + \tau_{cw,\alpha}$$

With

$\underline{w}$  the vertical component of the quasi-Eulerian velocity

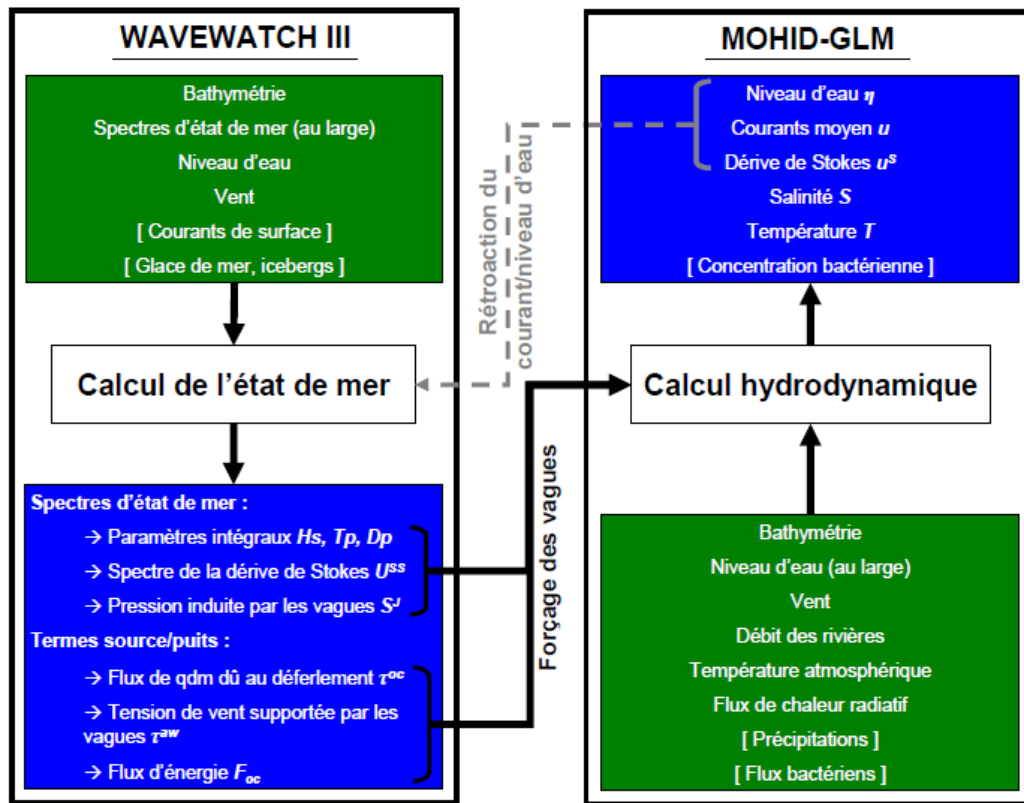
$W_s$  the vertical components of the Stokes drift (given by the wave model)

$\tau_{a,\alpha}$  = total wind stress

$\tau_{aw,\alpha}$  = wind stress supported by waves (given by the wave model)



# Implementation of MOHID-GLM



# Implementation of MOHID-GLM

## MOHID Water modifications

- Conservative formulation
- Reading of additional forcing variables (*Module Waves*)
- Compute  $U_s$ ,  $V_s$  from the frequency spectrum of the Stokes Drift (*Module Waves*)
- Add  **$U_s$ ,  $V_s$**  in advection terms (*Module Hydrodynamic*)
- Add contribution of  **$J$  and  $F_d$**  in the momentum equation (*Module Hydrodynamic*)
- Modify **boundary conditions** (*Modules Hydrodynamic, InterfaceWaterAir, InterfaceSedimentWater*)
- Modify surface boundary conditions for **TKE equation** in the k-epsilon model (*Modules GOTM and InterfaceWaterAir*)

→ For detailed discretization see: Delpey 2012.

Mass conservation:

$$\frac{\partial \eta}{\partial t} = - \frac{\partial}{\partial x_\alpha} \overbrace{\left( \int_{-h}^{\eta} (u_\alpha + \bar{u}_\alpha^S) dz \right)}^{A_1}.$$

Horizontal momentum conservation:

$$\begin{aligned} \frac{\partial u_\alpha}{\partial t} + \overbrace{\frac{\partial [u_\alpha(u_\beta + \bar{u}_\beta^S)]}{\partial x_\beta}}^{A_2} + \frac{\partial [u_\alpha(w + \bar{w}^S)]}{\partial z} \\ = - \frac{1}{\rho_0} \frac{\partial p^a}{\partial x_\alpha} + (-g + b(\eta)) \frac{\partial \eta}{\partial x_\alpha} + \int_z^\eta \frac{\partial b}{\partial x_\alpha} dz - \overbrace{\frac{\partial S^J}{\partial x_\alpha}}^B + \overbrace{\bar{u}_\beta^S \frac{\partial u_\beta}{\partial x_\alpha}}^C \\ + \frac{\partial}{\partial x_\beta} \left( K_H \frac{\partial u_\alpha}{\partial x_\beta} \right) + \frac{\partial}{\partial z} \left( K_V \frac{\partial u_\alpha}{\partial z} \right). \end{aligned}$$

Vertical advection velocity:

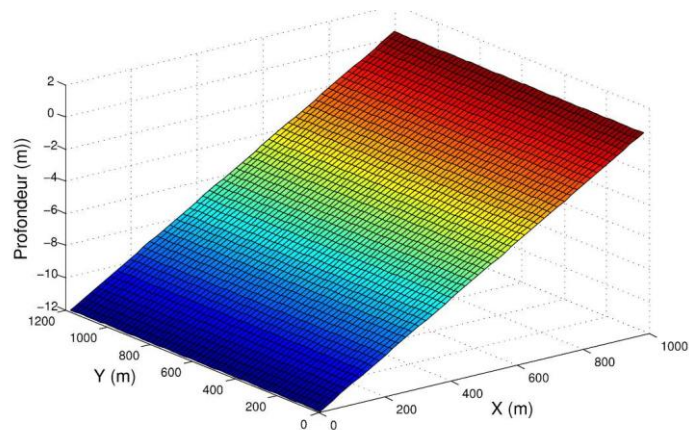
$$\bar{w}^L = w + \bar{w}^S = - \frac{\partial}{\partial x_\alpha} \overbrace{\left( \int_{-h}^z (u_\alpha + \bar{u}_\alpha^S) dz \right)}^{A_3}.$$

Tracer equation:

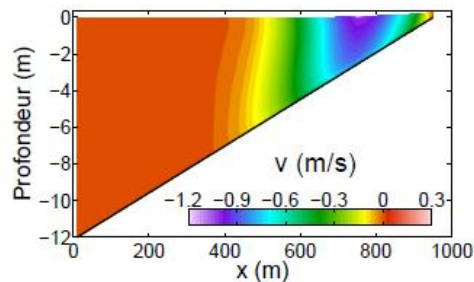
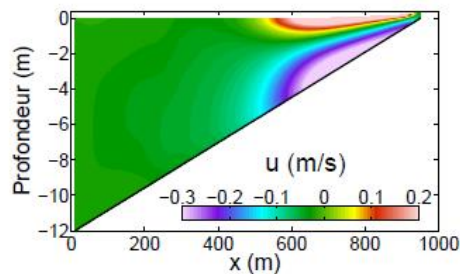
$$\frac{\partial C}{\partial t} + \overbrace{\frac{\partial [(u_\alpha + \bar{u}_\alpha^S)C]}{\partial x_\alpha}}^{A_4} + \frac{\partial [(w + \bar{w}^S)C]}{\partial z} = \frac{\partial}{\partial x_\alpha} \left( \frac{K_H}{\sigma_C} \frac{\partial C}{\partial x_\alpha} \right) + \frac{\partial}{\partial z} \left( K_T \frac{\partial C}{\partial z} \right) + S_C.$$

# Validation of MOHID GLM

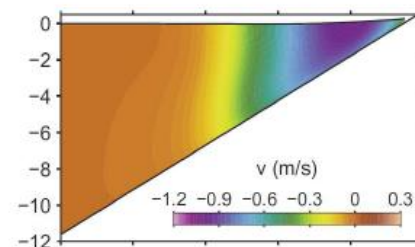
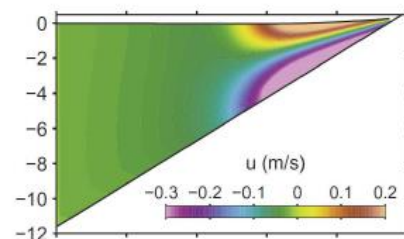
## Haas & Warner 2009 case



► Solution de MOHID-GLM ( $z_{0,s} = 0.2H_S$ )



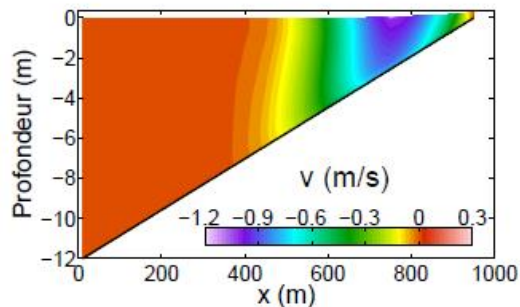
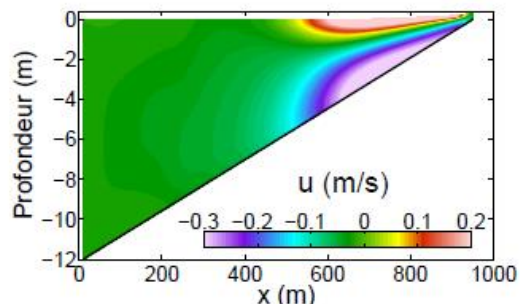
► Solution de ROMS [Uchiyama et al., 2010]



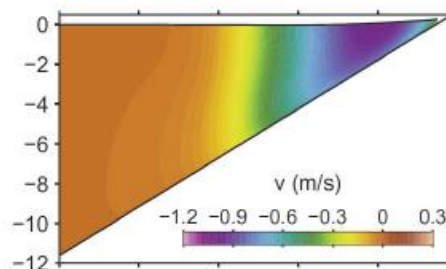
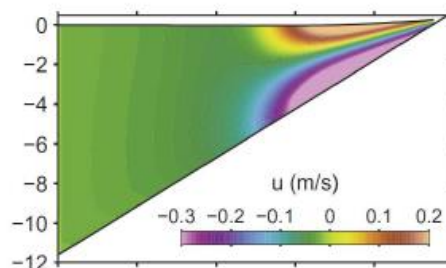
# Validation of MOHID GLM

## Haas & Warner 2009 case

► Solution de MOHID-GLM ( $z_{0,s} = 0.2H_S$ )

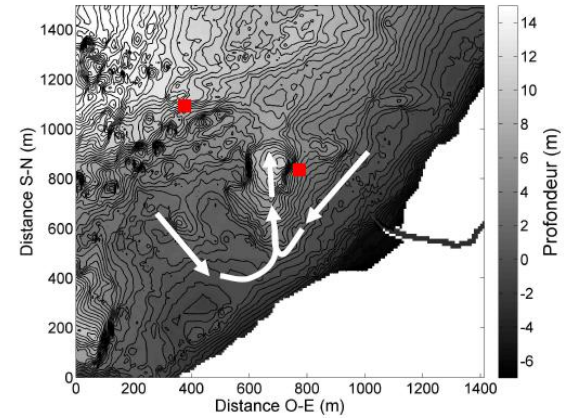
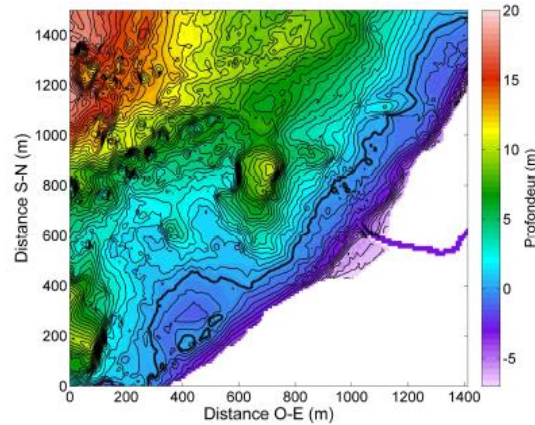


► Solution de ROMS [Uchiyama et al., 2010]



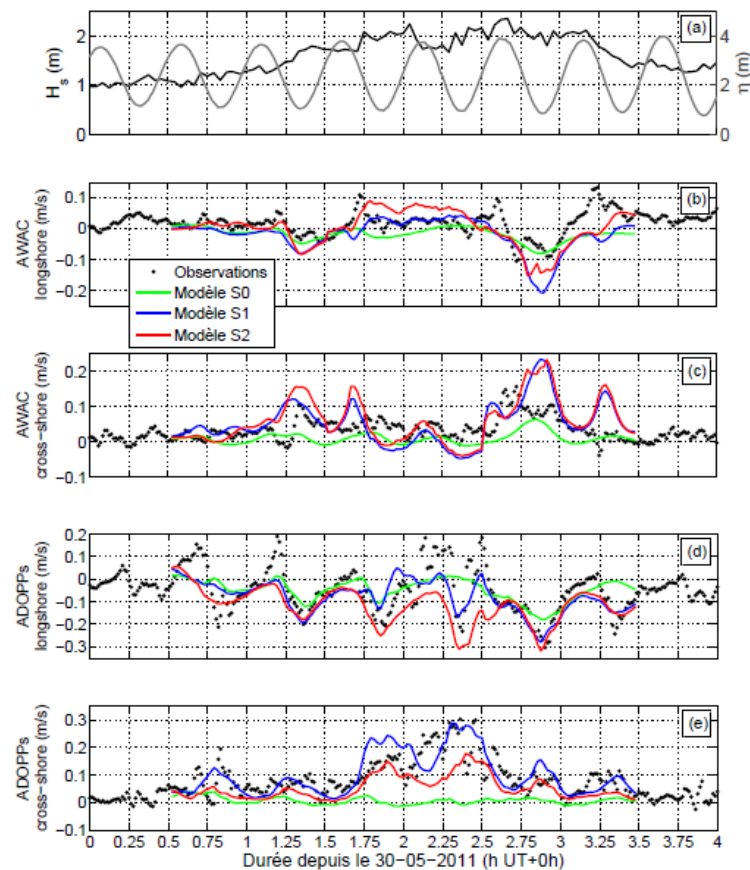
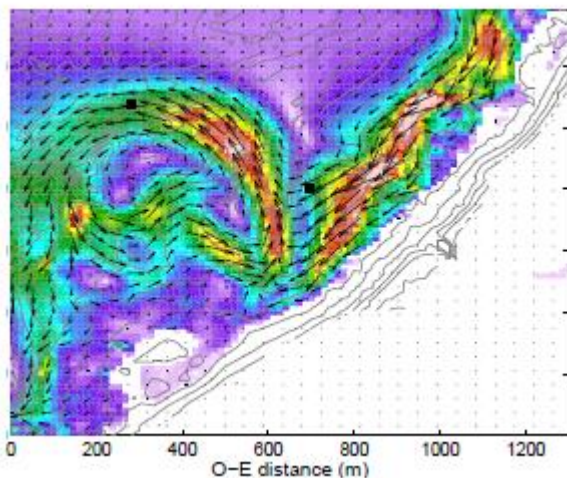
# Real case application

## Application to the Uhabia beach, SW France



# Real case application

## Application to the Uhabia beach, SW France



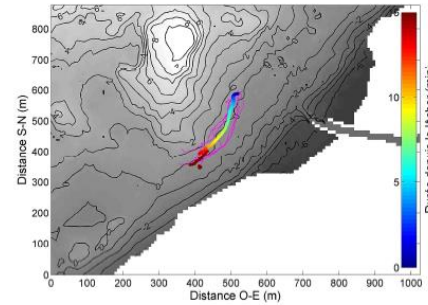


# Real case application

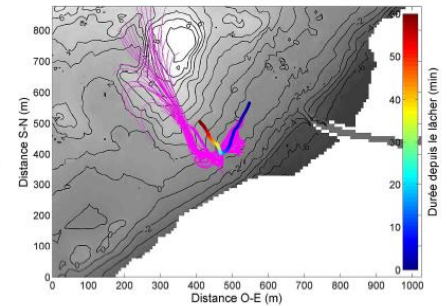
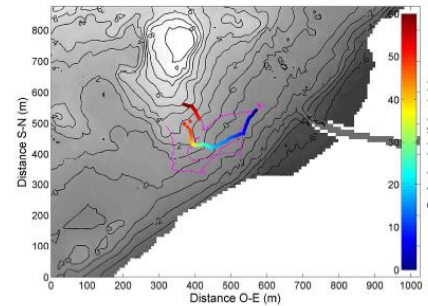
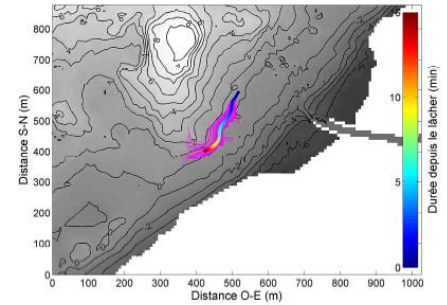
## Application to the Uhabia beach, SW France



Drifter observation



Model



# A (very) simplified formulation

## Exponential vertical decrease of radiation stress

$$S_{ij}'(x, y, z) = \frac{ke^{kz}}{e^{k\eta} - e^{-kh}} S_{ij}(x, y)$$

k = wave number, h = depth,  $\eta$  = free surface elevation

- No theoretical justification → « Empirical »
- Principle: consistent with barotropic balance + having a vertical distribution « a bit more plausible » than using homogeneous vertical distribution of wave radiation stress
- Allows to produce some features like undertow → See e.g. Franz et al. 2017



# MOHID-GLM : code developments for 3D waves-current interactions

Implementation of the glm2-RANS equations by Ardhuin et al. 2008

MOHIDing workshop – 7-8 June, 2018 – Lisbon, Portugal

**Matthias Delpey - SUEZ**

Center Rivages Pro Tech  
matthias.delpey@rivagesprotech.fr

